

**Remarks:**

Claims 1-3 and 6-8 are amended and claims 9-14 added herein. Upon entry of this amendment, claims 1-14 will be pending in the subject Application.

A copy of the entire specification showing the amendments presented herein is attached per the Examiner's request.

**Claims 1-8 – Section 112**

Applicant respectfully requests reconsideration of the rejection of claims 1-8 under 35 U.S.C. § 112, first paragraph, as containing subject matter which was not described in the specification in such a way as to enable skilled in the art to make and/or use the invention. The amendment to claims 1-8 deletes "to display a stereoscopic image" (claims 1, 6, and 7) and "displaying a stereoscopic image" (claim 8). The Office Action draws a distinction between an apparatus' ability to display a stereoscope image and an apparatus' ability to display an image that is perceived as stereoscopic by the viewer. Although Applicant respectfully disagrees with the distinction and application of the distinction as the basis for a rejection, the amendments to the subject claims render the point moot and the rejection improper. Accordingly, Applicant respectfully requests that the rejection be withdrawn.

**Claims 1-8 – Objection**

Applicant respectfully requests reconsideration of the objection to claims 1-8. The amendment to claims 1-8 deletes "arbitrary phase distribution" and "stereoscopic image." The Office Action asserts that because there is no logical connection between "arbitrary phase distribution" and the "stereoscopic image," the claims are confusing and indefinite. As an initial matter, a claim that the Examiner finds unclear and indefinite should not be objected to because objections address improper claim form (e.g., improper dependency), not improper claim substance. See M.P.E.P. § 706.01 (distinguishing rejections and objections). Further, Applicant respectfully disagrees with the assertion that the scope of the claims is confusing and indefinite. In any event, the amendments to the subject claims render the objection (and any similarly based Section 112, second

paragraph, rejection) improper. Accordingly, Applicant respectfully requests that the objection be withdrawn.

#### Claims 1-6 – Section 103

Applicant respectfully requests reconsideration of the rejection of claims 1-6 under 35 U.S.C. § 103(a) as being unpatentable over U.S. Patent No. 5,982,553 (Bloom) in view of U.S. Patent No. 5,694,235 (Kajiki) and U.S. Patent No. 6,307,663 (Kowarz). As amended, claims 1-5 recite a one-dimensional spatial modulator including one-dimensionally arrayed elements having top surfaces, the elements being independently driven such that the entire top surface of each element selectively moves upward and downward during operation of the display apparatus. As amended, claim 6 recites a Grating Light Valve device having a plurality of ribbon-like elements that have top surfaces, the Grating Light Valve being configured to generate a phase distribution by independently driving each ribbon-like element so that all of the top surface of each elements selectively moves up and down during operation of the display apparatus.

The amendments to claims 1-6 are supported by the specification. For instance, exemplary elements or ribbons are designated by reference number 11 in Figs. 1 and 2. The specification states phase distributions are generated “by the *independent* driving of *each* ribbon 11 of a GLV 10” (page 11, lines 4-7)(emphasis added), which enables various types of signal processing (page 12, lines 17-20). The specification further identifies a function describing the manner in which each element is separately driven (page 11, lines 16-25) in the “x” direction (e.g., from right to left in Figs. 1 and 2). Because each element includes a top surface and moves up and down as a whole (see e.g., page 12, lines 6-8, and Figs. 1 and 2), the entire top surface (e.g., the right-most surface in Figs. 1 and 2) of each element moves up and down (e.g., right and left in Figs. 1 and 2) during operation.

Bloom discloses a display grating light valve have active ribbons 12, 12A separated by fixed ribbons 18, 18A. Kajiki discloses a 3-D recording/reproducing system including a modulator 19. Kowarz discloses a light modulator wherein portions of ribbon elements 23a-23d move up and down while portions intermediate the moving portions (i.e., portions positioned above intermediate supports 27) remain fixed. Bloom, Kajiki, and

Kowarz, individually and in combination, fail to show or suggest elements independently driven such that all of the top surfaces of the elements selectively move upward and downward, as claimed.

Because the references, individually or in combination, do not show or suggest every claimed feature, the rejection is improper. Accordingly, Applicant respectfully requests the rejection be withdrawn.

#### Claims 7 and 8 – Section 103

Applicant respectfully requests reconsideration of the rejection of claims 7 and 8 under 35 U.S.C. § 103(a) as being unpatentable over Bloom in view of Kajiki. As amended, claim 7 recites means for spatially modulating the coherent light in a one-dimensional direction, wherein the means for spatially modulating is controlled in part according to a Fourier transformation function, and means for scanning the modulated light in a direction orthogonal to the one-dimensional direction and in a direction parallel to the one-dimensional direction.

As amended, claim 8 recites spatially modulating the coherent light in a one-dimensional direction in accord with a Fourier transformation function.

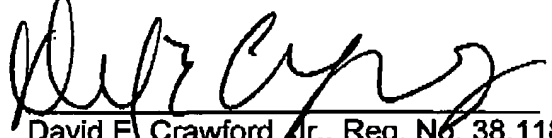
Bloom discloses a display grating light valve have active ribbons 12, 12A separated by fixed ribbons 18, 18A. Kajiki discloses a 3-D recording/reproducing system including a modulator 19. The references fail, individually and in combination, to show or suggest controlling the means for spatially modulating in part according to a Fourier transformation function and means for scanning the modulated light in a direction orthogonal to the one-dimensional direction and in a direction parallel to the one-dimensional direction (claim 7) or to show or suggest spatially modulating the coherent light in a one-dimensional direction in accord with a Fourier transformation function (claim 8).

Because the references, individually or in combination, fail to show or suggest every claimed feature, the rejection is improper. Accordingly, Applicant respectfully requests the rejection be withdrawn.

Conclusion

As it is believed that the Application is in condition for allowance, a favorable action and Notice of Allowance are respectfully requested.

Respectfully submitted,



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## STEREOSCOPIC IMAGE DISPLAY APPARATUS

### RELATED APPLICATION DATA

This application claims priority to Japanese Patent  
5 Application JP 2000-358207, and the disclosure of that  
application is incorporated herein by reference to the extent  
permitted by law.

### BACKGROUND OF THE INVENTION

#### 10 1. Field of the Invention

The present invention relates to a stereoscopic image  
display apparatus for displaying a stereoscopic image.

#### 2. Description of the Related Art

15 Various kinds of display apparatus for displaying  
planar images (two-dimensional images) by radiating light  
have hitherto been put to practical use. For example, a  
liquid crystal panel and a digital micro-mirror device (DMD)  
have been used as a spatial modulator for modulating light  
20 to be projected according to a planar image to be displayed  
in such a display apparatus.

Moreover, research and development of diffraction  
gratings that can freely be driven by micro-machines have been  
25 proceeding in recent years. Bloom et al (U.S. Pat. No.  
5,311,360) discloses a display apparatus using such a  
diffraction grating as a spatial modulator for modulating  
light to be projected ~~according to a displaying image was~~  
~~submitted and has been widely noticed.~~

The A micro-machine type diffraction grating ~~to be used~~  
as a spatial modulator ~~like this~~ is generally called ~~as~~ a  
Grating Light Valve (GLV) ~~[[,]]. GLVs have and such a~~  
5 ~~diffraction grating has~~ features ~~such that it can~~ allowing  
them to be operated at a higher speed and can be manufactured  
at a lower cost by using various ~~kinds of~~ semiconductor  
manufacturing techniques ~~in comparison with a~~ compared to  
liquid crystal ~~panel panels~~ and ~~a DMD~~ DMDs that have hitherto  
10 been used as a spatial modulator.

Accordingly, it is expected that a display apparatus  
can display a clear and bright image without any discontinuity  
and can be realized at a low cost when the display apparatus  
15 is configured by the use of the GLV.

On the other hand, as for display apparatuses for  
displaying stereoscopic images (three-dimensional images),  
though the display apparatuses have hitherto been realized  
20 by the use of various systems, many of them have various  
restrictions such that visual fields are limited within  
narrow ranges or that special glasses are needed to see, and  
they have not been put to full-scale practical use yet.

25 Accordingly, various technologies making it possible  
to display stereoscopic images in real time by the use of  
various hologram techniques have been proposed in recent  
years. As an example of such proposals, there is a display  
apparatus (U.S. Pat. No. 5,172,251) that uses acousto-optic

devices controlled by a computer apparatus or the like as one-dimensional hologram devices (hereafter called computer generated hologram (CGH)) and displays stereoscopic images by scanning one-dimensional stereoscopic images generated by  
5 the CGH in horizontal directions and vertical directions.

#### SUMMARY OF THE INVENTION

~~However, in the case where~~ Where stereoscopic images are displayed by the use of the acousto-optic devices in the  
10 way described above, for example, the acousto-optic devices are used as one-dimensional hologram devices by creating a refractive index distribution by the input of ultrasonic waves according to displaying images. However, the displayed images may be distorted as if the displayed image  
15 is flowing due to the nature of the ultrasonic waves to be traveling waves. Accordingly, it is necessary to correct the "flowing" distortion of displayed images by the use of, for example, a polygon mirror or a galvano-mirror. In this case, ~~there are problems presented include such that~~ the whole  
20 structure of the display apparatus ~~becomes~~ being complicated[[,]] and ~~further that it is needed~~ the need to adjust the timing of the correction to be extremely accurate lest time lags ~~should~~ will be generated.

25 Moreover, devices other than the acousto-optic devices are ~~so far~~ difficult to ~~obtain~~ use as a spatial modulator that can operate at a high speed and perform ~~the modulation~~ modulation with an abundant amount of information, ~~both the speed and the amount being sufficient~~ to display stereoscopic

images, ~~in a display apparatus for displaying the~~  
~~stereoscopic images.~~ The Further, conventional  
acousto-optic devices ~~have shortcomings of that they are~~  
expensive and ~~that~~ high voltages are necessary ~~for driving~~  
5 to drive them.

~~There is another problem. Enormous~~ An enormous amount  
of information is required for displaying stereoscopic images  
because it ~~becomes~~ is necessary to display precise  
10 information in three-dimensional directions. It is not  
practical ~~at present~~ to control such enormous amount of  
information with conventional devices. Moreover, because  
the amount of information to display a stereoscopic image  
increases by leaps and bounds as the sizes of the images to  
15 be displayed become large, display of a large size  
stereoscopic images becomes very difficult. ~~Besides~~ Also,  
in the case where stereoscopic images are displayed as moving  
picture in real time, the necessary amount of information  
further jumps up by leaps and bounds[[,]] and it ~~becomes~~ is  
20 necessary to process an enormous amount of information at  
extremely high speed.

Although various kinds of display apparatuses for  
displaying stereoscopic images have hitherto been proposed,  
25 such display apparatuses have many problems, such as those  
mentioned above, and ~~the display apparatuses~~ are not put to  
practical use yet.

The present invention is made in consideration of the



aforesaid situation and problems. It is desired to provide a stereoscopic image display apparatus capable of displaying stereoscopic images at a higher speed and with a simpler structure than can be manufactured at a lower cost.

5

According to ~~an~~ one embodiment of the present invention, ~~a stereoscopic image display apparatus is provided. The~~ stereoscopic image display apparatus comprises a light source radiating light of a wavelength in a predetermined wavelength range, ~~an~~ a one-dimensional spatial modulator including  
10 one-dimensionally arrayed elements that are independently driven to generate an arbitrary phase distribution[[]], and a scan unit scanning the light from the light source to a predetermined direction, the light having entered into the  
15 one-dimensional spatial modulator and having been modulated therein.

The stereoscopic image display apparatus according to the present embodiment, ~~which configured as above,~~ uses the  
20 one-dimensional spatial modulator including the independently driven elements as a spatial modulator for modulating light to be projected. Because such a one-dimensional spatial modulator may be operated at ~~a~~ an extremely high speed, stereoscopic images may be displayed  
25 based on a sufficiently abundant amount of information. Moreover, because the stereoscopic image display apparatus displays stereoscopic images by the use of light modulated by the one-dimensional spatial modulator, the overall structure of the apparatus may be simplified, and the

manufacturing cost thereof may be lowered. Moreover, the apparatus may express a stereoscopic effect without any special equipment such as special glasses to view stereoscopic image.

5

Moreover, the stereoscopic image display apparatus of the present embodiment displays stereoscopic images by scanning and radiating the light modulated by the one-dimensional spatial modulator. Thereby, for example, the stereoscopic images may be displayed with only horizontal parallax of the stereoscopic images to be displayed by the renunciation of vertical parallax. By displaying of the stereoscopic images with one directional parallax in such a way, the increase of a necessary amount of information may be suppressed, and an amount of information and a processing time, both necessary for displaying stereoscopic images, may be decreased to a practical level.

Even when the stereoscopic images are displayed with only horizontal parallax as described above, stereoscopic effects may fully be expressed because two human eyes are arrayed in a horizontal direction and more insensitive to vertical parallax than horizontal parallax.

In the stereoscopic image display apparatus according to the present embodiment, the scan unit may scan the light modulated by the one-dimensional spatial modulator in a direction perpendicular to the arraying direction of the elements of the one-dimensional spatial modulator.

Accordingly, a larger ~~size of the~~ stereoscopic image may be displayed and a wider viewing field may be ensured ~~by projecting the scanning light that is modulated with the one-dimensional spatial modulator and scanned with the scan~~  
5 ~~unit into the perpendicular direction to the arraying direction of the elements since~~ because the one-dimensional spatial modulator with the individually driven elements may be operated in a sufficiently fast speed.

10        According to another embodiment of the present invention, there is provided a stereoscopic image display apparatus comprising: a light source radiating light of a wavelength in a predetermined wavelength range; a Grating Light Valve device that can independently drive each  
15 ribbon-like element to generate an arbitrary phase distribution of the light; a collimator lens making the light modulated by the Grating Light Valve device into parallel ray; a scan unit scanning the parallel ray from the collimator lens; a lens performing Fourier transformation on the scanned  
20 ray; and a diffuser panel diffusing the ray Fourier transformed by the lens.

      According to the above mentioned embodiment of the present invention, the stereoscopic image display apparatus  
25 capable of displaying stereoscopic images ~~in~~ at a higher speed may be realized at a lower cost with a simpler structure. Moreover, according to the above mentioned embodiment, an amount of information and a processing time, both being necessary for displaying a stereoscopic image, may be

decreased thereby enabling the moving picture display of stereoscopic images in real time.

#### BRIEF DESCRIPTION OF THE DRAWINGS

5           The other objects, features, and advantages of the present invention will become more apparent from the following description including ~~of the presently preferred~~ exemplary embodiments of the invention ~~taken~~ in conjunction with the accompanying drawings, in which:

10           Fig. 1 is a ~~mimetic diagram~~ schematic showing ~~a state such that light enters into a GLV being an example of incident light waves approaching the GVL of a spatial modulator of the~~ present invention;

15           Fig. 2 is a ~~mimetic diagram~~ schematic showing light waves ~~a state such that the light entered into after being modulated by the GLV being an example of the spatial modulator of the present invention is modulated and reflected;~~

20           Fig. 3 is a ~~mimetic diagram~~ schematic perspective ~~for explaining the principle of the present invention by~~ illustrating the scanning of the light modulated by the GLV ~~in a predetermined direction;~~

25           Fig. 4 is a ~~schematic diagram of a display apparatus shown as an example of the structure~~ perspective of the stereoscopic image display apparatus according to the present invention;

          Fig. 5 is a ~~schematic diagram for illustrating the rotation directions of a first and a second galvano mirrors of the display apparatus~~ of the stereoscopic image display apparatus shown in Fig. 4 from another perspective;

Fig. 6 is a ~~mimetic diagram~~ schematic showing an example of a ~~state such that~~ scanning directions of the laser beams modulated to one-dimensional wavefronts scan in a projection plane on which stereoscopic images are projected by in the display apparatus;

Fig. 7 is a ~~mimetic diagram~~ schematic showing another example of a ~~state such that~~ scanning directions of the laser beams modulated to one-dimensional wavefronts scan in a projection plane on which stereoscopic images are projected by in the display apparatus;

Fig. 8 is a ~~schematic~~ block diagram showing a control circuit provided in the display apparatus; and

Fig. 9 is a schematic perspective ~~view of a mirror array~~ shown as an example of a display apparatus having a scan mechanism including a mirror arra provided in the display apparatus.

#### DETAILED DESCRIPTION OF THE ~~PREFERRED EMBODIMENTS~~ INVENTION

Hereinafter, the attached drawings are referred to while a ~~preferred embodiment~~ embodiments of the stereoscopic image display apparatus according to the present invention are described ~~in detail~~.

One of the features of a first embodiment of the present ~~embodiment~~ invention is to use a micro-machine type one-dimensional spatial modulator as a spatial modulator for modulating light to be projected. Specifically, as such a spatial modulator, a micro-machine type diffraction grating may be used. The micro-machine type diffraction grating is

generally called as a Grating Light Valve (GLV) when it is used as a spatial modulator.

~~The principle employed in the present embodiment is described in the following before the embodiment of the present invention is described.~~

A GLV comprises a plurality of minute ribbons formed on a substrate. The ribbons may be fabricated with various semiconductor manufacturing techniques. Each ribbon is configured to be able to ~~arbitrary~~ arbitrarily ascend and descend ~~by~~ in response to actuation from a piezoelectric device or the like. The GLV with such ribbon structure may be operated to dynamically drive each ribbon to vary its height while light with a predetermined wavelength range is irradiated thereto, thereby constituting a phase type diffraction grating as a whole. That is, the GLV generates the  $\pm 1^{\text{st}}$  order (or higher order) diffracted light ~~by receiving irradiation of the light from the incident irradiant light~~ received.

Accordingly, an image may be displayed by the following operations: irradiation of light to the GLV; shielding of the 0<sup>th</sup> order diffracted light; and driving each ribbon of the GLV ~~upwardly upward and downwardly downward~~ upward and downward so as to have the diffracted light blink.

Various display apparatuses for displaying planar images (two-dimensional images) by utilizing the aforesaid

characteristics of a GLV have hitherto been ~~introduced~~  
introduced. When a conventional display apparatus displays  
a constituent unit (hereinafter referred to as a pixel) of  
a planar image to be displayed, about six ribbons are used  
5 for displaying ~~one~~ the pixel. Furthermore, in a group of  
ribbons corresponding to one pixel, ~~adjoining~~ adjacent  
ribbons are made to ascend or descend ~~alternately~~.

However, if each ribbon in a GLV ~~may~~ is independently  
10 ~~be~~ wired to be driven separately, an arbitrary  
one-dimensional phase distribution may be generated. The  
GLV structured in such a way may be regarded as a reflection  
type one-dimensional phase type hologram.

15 In the present embodiment, the GLV structured as a  
reflection type one-dimensional phase type hologram in the  
aforesaid way is used as the micromachine type  
one-dimensional spatial modulator. That is, for example, as  
shown in Fig. 1, an arbitrary phase distribution has been  
20 generated in advance by the independent driving of each ribbon  
11 of a GLV 10. When light with a predetermined wavelength  
range the phase of which is aligned enters into the GLV 10  
from the direction indicated by an arrow in Fig. 1, the  
incident light is modulated and reflected. Then, as shown  
25 in Fig. 2, an arbitrary one-dimensional wavefront may be  
formed.

~~Hereupon, a specific example in the case where  
stereoscopic images are displayed by the use of such GLV is~~

~~described.~~ In the case where a stereoscopic image is displayed by the use of the GLV in which a plurality of ribbons are one-dimensionally arrayed, each ribbon of the GLV is driven as follows: the Fourier transformation of a function  $a(x) : A(X) = H(X) \exp[i\phi(X)]$  is calculated when an amplitude of the one-dimensional wavefront generated by the GLV is expressed by the  $a(x)$  as a function in an  $x$ -direction $[[;]]$  and then each ribbon of the GLV is driven in such a way that a phase difference corresponding to the phase component  ~~$\phi(x)$~~   $\phi(X)$  is given to the reflected light.

In order to be more precise, it is desirable to modulate the amplitude component  $H(X)$  as well. Accordingly, a more accurate three-dimensional display may be realized. Incidentally, the display apparatus may still be able to display a stereoscopic image with sufficient stereoscopic effects even if the amplitude component  $H(X)$  is set to be constant.

20

When the ribbon in the GLV descends by a depth  $[[\emptyset]]$   $\Psi$  from its default position, a change of  ~~$2\emptyset$~~   $2\Psi$  is generated in the optical path length for the reflected light. Accordingly, the phase difference generated by this change is  ~~$4\emptyset/\lambda$~~   $4\Psi/\lambda$  where  $[[\emptyset]]$   $\lambda$  designates the wavelength of the light.

25

Because ~~the~~ analog modulation of the GLV is possible, a desired phase difference may be given to the reflection



light by precise analog driving of the GLV. However, when  
a display apparatus ~~is structured by the use of~~ has such a  
GLV, it is practical to use a discrete calculation method such  
as the fast Fourier transformation. Accordingly, it is  
5 practical to discretely drive each ribbon of the GLV based  
on a digital signal ~~discretely~~, and thereby ~~enabling easily~~  
allowing for various kinds types of signal processing ~~easy~~.

Another embodiment in accordance with the present  
10 invention is characterized by displaying stereoscopic images  
by the use of, for example, a technique shown in Fig. 3 on  
the basis of the aforesaid principle. As shown in Fig. 3,  
a GLV 20 in which a plurality of ribbons are one-dimensionally  
arrayed generates one one-dimensional wavefront after  
15 another. The generated wavefronts are scanned in a vertical  
direction by a scan mechanism comprising, for example, a  
galvano-mirror 21. That is, by rotating the galvano-mirror  
21 in a direction shown by an arrow A in Fig. 3, a plurality  
of wavefronts 22a, 22b, 22c are radiated in such a way that  
20 they are arranged in the vertical direction. Thereby, a  
stereoscopic image may be displayed. It is desirable to  
provide a one-dimensional diffuser panel 23 in the vicinity  
of the stereoscopic image to be displayed. By the diffuser  
panel 23, a vertical visual field may be enlarged slightly,  
25 and discontinuities between the wavefronts 22a, 22b, 22c are  
made to be inconspicuous. Accordingly, more natural  
stereoscopic effects may be expressed. Although horizontal  
parallax may be sufficiently achieved by the technique shown  
in Fig. 3, it is difficult to also obtain vertical parallax.

This difficulty is addressed in the following.

~~That is, as shown in Fig. 3, a CLV 20 in which a plurality of ribbons are one dimensionally arrayed generates an one dimensional wavefront one after another. The generated wavefronts are scanned in a vertical direction by a scan mechanism comprising, for example, a galvano mirror 21. That is, by the rotation of the galvano mirror 21 in a direction shown by an arrow A in Fig. 3, a plurality of wavefronts 22a, 22b, 22c are radiated in such a way that they are arranged in the vertical direction. Thereby, a stereoscopic image may be displayed.~~

~~As shown in Fig. 3, it is desirable to provide an one dimensional diffuser panel 23 in the vicinity of a stereoscopic image to be displayed. By the diffuser panel 23, a vertical visual field may be enlarged slightly, and discontinuities between the wavefronts 22a, 22b, 22c are made to be inconspicuous. Accordingly, more natural stereoscopic effects may be expressed.~~

~~Now, in the case where stereoscopic images are displayed by the vertical scanning of one dimensional wavefronts with utilizing the technique shown in Fig. 3, horizontal parallax may sufficiently be secured, but it becomes difficult to obtain vertical parallax as well. Accordingly, such difficulty is addressed in the following.~~

~~When a display apparatus is structured by the use of~~

includes a diffraction grating such as a GLV or a hologram, the relations expressed by the following Equation 1 and Equation 2 are satisfied, where the maximum spatial frequency of the diffraction grating, the shortest period of the grating, a reproduced wavelength, and a diffraction angle (the diffraction angle influences the extent of a visual field) are respectively designated by  $f_h$ ,  $[\underline{E}]/\underline{\lambda}$ ,  $[\underline{e}]/\underline{\lambda}$ , and  $[\underline{e}]/\underline{\theta}$ .

$$\begin{aligned} f_h &= 1/\underline{E} \quad f_h = 1/\underline{\lambda} \quad \dots \text{ (Equation 1)} \\ f_e &= \sin \theta \quad f_h \underline{\lambda} = \sin \theta \quad \dots \text{ (Equation 2)} \end{aligned}$$

According to the sampling theorem, the minimum sampling frequency  $f_s$  may be expressed ~~to meet to~~ by the following Equation 3.

$$f_s = 2f_h \quad \dots \text{ (Equation 3)}$$

Accordingly, a sample number N necessary for reproducing ~~an~~ a one-dimensional stereoscopic image having a horizontal length d may be expressed ~~to meet~~ by the following Equation 4.

$$N = d \cdot f_s = (2d \cdot \sin \theta) / \underline{e} \quad N = d \cdot f_s = (2d \cdot \sin \theta) / \underline{\lambda} \quad \dots$$

(Equation 4)

Moreover, when the vertical resolution of the display apparatus is designated by L, the total number  $N_h$  of the samples constituting one stereoscopic image may be expressed by the following Equation 5 in the case where the stereoscopic

image is displayed by the technique shown in Fig. 3, namely when L pieces of the one-dimensional type diffraction gratings are vertically arranged.

5 
$$N_h = dL \cdot f_s = (2dL \cdot \sin \theta) / \lambda \quad N_h = dL \cdot f_s = (2dL \cdot \sin \theta) / \lambda \quad \dots$$
  
(Equation 5)

In order to secure the vertical parallax, a total number  $N_{hv}$  of the samples necessary for constituting one stereoscopic image may be expressed by the following Equation 6 where the vertical length of the stereoscopic image is designated by w.

15 6) 
$$N_{hv} = (2dw \cdot \sin^2 \theta) / \lambda^2 \quad N_{hv} = (2dw \cdot \sin^2 \theta) / \lambda^2 \quad \dots$$
 (Equation 6)

As being apparent can be seen by the comparison of comparing Equation 5 and Equation 6, a required amount of information (the number of samples) remarkably increases when achievement of both the horizontal parallax and the vertical parallax are tried to be secured, compared to when in comparison with that in the case where only the horizontal parallax is secured. For example, when the diffraction angle  $\theta$  is 30 degrees and the reproduced wavelength  $\lambda$  is 0.5  $\mu\text{m}$ , the total number  $N_{hv}$  of required samples is  $2dw \times 10^{12}$  according to Equation 6. Further, when the horizontal length d and vertical length w of a stereoscopic image to be displayed are 100 mm, the total number  $N_{hv}$  of samples necessary for displaying one stereoscopic image is  $2 \times 10^{10}$ . That is, 20

G bits (gigabits) of information becomes necessary to display  
a single stereoscopic image. Moreover, for example, if 30  
stereoscopic images are to be displayed every second for  
displaying moving picture images, 600 G bits (75 G bytes) of  
5 information becomes necessary every second.

~~More specifically, when the diffraction angle  $\theta$  is set~~  
~~to be 30 degrees and the reproduced wavelength  $\lambda$  is set to~~  
~~be 0.5  $\mu\text{m}$ , the total number  $N_{hw}$  of the required samples is~~  
10  ~~$2dw \times 10^{12}$  in conformity with Equation 6. Hereupon, when the~~  
~~horizontal length  $d$  and the vertical length  $w$  of a~~  
~~stereoscopic image to be displayed are severally set to be~~  
~~100 mm, the total number  $N_{hw}$  of the samples necessary for~~  
~~displaying one stereoscopic image is  $2 \times 10^{10}$ . That is, the~~  
15 ~~amount of information of 20 G bits becomes necessary for~~  
~~displaying one piece of stereoscopic image. Moreover, if 30~~  
~~stereoscopic images are to be displayed every second for~~  
~~displaying moving picture image, the amount of information~~  
~~of 600 G bits (75 G bytes) becomes necessary every second.~~

20

~~Incidentally, the amount of information of 600 G bits~~  
~~of information is equal to an the same amount of information~~  
~~required when the moving picture image is pictures are~~  
~~displayed with using monochromatic and no-gradation images.~~  
25 ~~If a color display with the three primary colors is to be~~  
~~performed desired, an the amount of information required is~~  
~~tripled. If eight levels of gradation is are to be used, eight~~  
~~times of the amount of information is further required.~~  
~~Furthermore, if displaying is performed on a 12-inch size~~

display apparatus, ~~an amount of information~~ seven times the  
amount of information or more is further needed. ~~Accordingly,~~  
~~signal~~ Signal processing dealing with such an enormous amount  
of information at a high speed is far from being put to  
5 practical use at present by conventional methods.

~~On the other hand, according~~ According to the present  
~~embodiment invention, by the use of~~ using the technique shown  
in Fig. 3, a stereoscopic image is displayed only by the  
10 horizontal parallax thereof by the relinquishment of, with  
the vertical parallax thereof being relinquished. In this  
case, ~~similarly similar to what have been that~~ described above,  
for example, when the diffraction angle  $[\theta]$  is set to be  
30 degrees and the reproduced wavelength  $[\lambda]$  is set to be  
15  $0.5 \text{ } [\mu\text{m}]$ , the total number  $N_{hv}$  of the required samples  
is  $2dL \times 10^6$  in accord conformity with Equation 5. If the  
horizontal length  $d$  and the vertical length  $w$  of a  
stereoscopic image to be displayed are ~~severally set to be~~  
100 mm and the vertical resolution  $L$  is set to be 1000, the  
20 total number  $N_h$  of the samples necessary for displaying one  
piece of stereoscopic image is  $2 \times 10^8$ . This amount of  
information is ~~1/100 in comparison with~~ 1/100<sup>th</sup> of the  
aforesaid total sample number  $N_{hv}$  ~~(i.e.,~~ (i.e.,  $2 \times 10^{10})$ .  
According to the present embodiment, using the technique  
25 shown in Fig. 3, it is possible to decrease the amount of  
information and processing time necessary for displaying a  
stereoscopic image at a practical level. Also, because two  
human eyes exist in a horizontal line, human eyes are less  
sensitive to vertical parallax than to horizontal parallax.

Thus, stereoscopic effects may fully be expressed in the case where a stereoscopic image is displayed by the use of the technique shown in Fig. 3, with its vertical parallax being relinquished.

5

~~According to the present embodiment using the technique shown in Fig. 3, it becomes possible to decrease an amount of information and a processing time, both being necessary for displaying a stereoscopic image, to a practical level.~~

10

~~Incidentally, even in the case where a stereoscopic image is displayed by the use of the technique shown in Fig. 3, with its vertical parallax being relinquished, because two human eyes exist in a horizontal line, human eyes are more insensitive to the vertical parallax than horizontal parallax, and thereby stereoscopic effects may fully be expressed.~~

15

Next, according to ~~still~~ another embodiment of the present invention, a display apparatus 30 shown in Fig. 4 is provided for displaying a stereoscopic image. The display apparatus 30 displays stereoscopic images by scanning and projecting light modulated by a micromachine type one-dimensional spatial modulator ~~by utilizing the aforesaid principle of the present~~ invention. The display apparatus 30 comprises a first laser oscillator 31a, a second laser oscillator 31b, and a third laser oscillator 31c that respectively emits a laser beam in the wavelength range of red, green and blue. Other types of coherent light sources such as solid state

20

25

laser device may be employed in place of the laser oscillators. The display apparatus 30 further comprises a GLV 32 for modulating the laser beams emitted from the laser oscillators 31a, 31b, 31c so as to form one-dimensional wavefronts  $W_r$ ,  $W_g$ ,  $W_b$  with desired phase distributions.

~~The display apparatus 30 comprises, as shown in Fig. 4, a first laser oscillator 31a, a second laser oscillator 31b and a third laser oscillator 31c that respectively emits a laser beam in each wavelength range of red, green and blue, respectively. The display apparatus 30 further comprises a GLV 32 for modulating the laser beams emitted from these laser oscillators 31a-31c so as to form one-dimensional wavefronts with respectively desired phase distributions.~~

~~Alternatively, other types of coherent light sources such as solid state laser device may be employed in place of the laser oscillators.~~

20

The GLV 32 is provided with three ribbon arrays 32a, 32b, 32c respectively formed from a plurality of minute ribbons that are one-dimensionally arrayed (in a straight line). In the GLV 32, each ribbon 32a, 32b, 32c is structured to be able to ascend and descend independently and ~~arbitrary~~ arbitrarily by use of a piezoelectric device or the like. ~~These~~ The ribbons 32a, 32b, 32c in the GLV 32 are independently driven by a control circuit that will be described later. ~~Moreover,~~



each ~~Each~~ ribbon array 32a, 32b, 32c of the GLV 32 is irradiated by a red laser beam, a green laser beam, or a blue laser beam that is respectively radiated from the first, the second, or the third laser oscillators 31a, 31b, 31c. That is, in the GLV 32, a ribbon array 32a for red, a ribbon array 32b for green, and a ribbon array 32c for blue are formed, and the red laser beam, the green laser beam, and the blue laser beam are selectively radiated. Then, the GLV 32 one-dimensionally modulates and reflects each laser beam to generate an arbitrary wavefront for each color: a red wavefront  $W_r$ , a green wavefront  $W_g$ , and a blue wavefront  $W_b$  shown in Fig. 4. Because the color wavefronts  $W_r$ ,  $W_g$ ,  $W_b$  travel through substantially the same optical path, they are collectively referred to as a laser beam in the following sections of the present specification.

~~That is, in the GLV 32, a ribbon array 32a for red, a ribbon array 32b for green, and a ribbon array 32c for blue are formed, and the red laser beam, the green laser beam or the blue laser beam is respectively radiated. Then, the GLV 32 one-dimensionally modulates and reflects each laser beam to generate an arbitrary wavefront at every color as red wavefront  $W_r$ , green wavefront  $W_g$  and blue wavefront  $W_b$  shown in Fig. 4. Because respective color wavefronts  $W_r$ ,  $W_g$ ,  $W_b$  that have been generated in such a way that they travel through substantially the same optical path, each color laser beam is named generically and simply as a laser beam in the following sections of the present specification.~~

Moreover, the display apparatus 30 comprises a collimator lens 33, a first galvano-mirror 34, a second galvano-mirror 35, a Fourier transformation lens 36, and an a one-dimensional diffuser panel 37, ~~all being~~ arranged in this order on an optical path of the laser beams reflected by the GLV 32. The collimator lens 33 allows the laser beams reflected by the GLV 32 to pass through to form parallel rays. The parallel rays leaving the collimator lens 33 are then incident on the first galvano-mirror 34. The first galvano-mirror 34 reflects the incident laser beams to make them incident on the second galvano-mirror 35. The second galvano-mirror 35 reflects the incident laser beams to make them incident on the Fourier transformation lens 36.

~~The collimator lens 33 allows the laser beams reflected by the GLV 32 to pass through to form parallel rays, and the parallel rays is incident on the first galvano-mirror 34. The first galvano-mirror 34 reflects the incident laser beams to make them incident on the second galvano-mirror 35. The second galvano-mirror 35 reflects the incident laser beams to make them incident on the Fourier transformation lens 36.~~

Rotations of the first and the second galvano-mirrors 34, 35 are controlled by a control circuit that will be described later. Assuming an xyz coordinate system as shown in Fig. 5, the first galvano-mirror 34 is controlled to rotate about the z-axis, and the second galvano-mirror 35 is controlled to rotate about the x-axis. That is, the first and the second galvano-mirrors 34, 35 have rotation axes

orthogonal to each other, and they are driven to rotate about respective rotation axes under the control of the control circuit.

5        ~~Accordingly, in the display apparatus 30, the laser beams, that have modulated by the GLV 32 and have one-dimensional wavefronts (linear wavefronts), are scanned by the first and the second galvano mirrors 34, 35 in such a way, for example, shown in Fig. 6. Fig. 6 schematically~~  
10        shows the scanning directions of the laser beams in a projection plane on which stereoscopic images are projected by the display apparatus 30. In the figure, the transverse direction is assumed as the horizontal direction, and the longitudinal direction is assumed as the vertical direction.  
15        That is, in the display apparatus 30, the first and the second galvano-mirrors 34, 35 are driven to rotate by the control circuit and, thereby, can scan the incident laser beams in the horizontal direction and the vertical direction, respectively.

20        ~~That is, in the display apparatus 30, the first and the second galvano mirrors 34, 35 are driven to rotate by the control circuit, and thereby they can scan the incident laser beams in the horizontal direction and the vertical direction, respectively.~~  
25        ~~respectively.~~

Because the laser beams modulated by the GLV 32 have one-dimensional wavefronts ~~in the display apparatus 30~~, stereoscopic images may be displayed by the scanning of the

laser beams only with the second galvano-mirror 35 in the direction perpendicular to the laser beam wavefronts[[,]] (i.e., in the vertical direction in Fig. 6), without using the first galvano-mirror 34. In this case, the horizontal  
5 length of the stereoscopic image to be displayed is restricted by the length of the ribbon arrays 32a, 32b, 32c formed on the GLV 32.

~~More specifically, when~~ When a GLV capable of  
10 displaying 1024 pixels is used as the GLV 32 in the display apparatus 30, ~~the number of~~ there are 6,144 ribbons ~~formed~~ in each ribbon array 32a, 32b, 32c in the GLV 32 ~~are severally 6144~~ (in the case where six ribbons are included in one pixel). ~~In the GLV 32, when~~ When  
15 it is assumed that an interval distance between two neighboring ribbons is 5 [[im]]  $\mu\text{m}$ , the horizontal length of a stereoscopic image capable of being projected by the display apparatus 30 ~~becomes~~ is about 30 mm unless a magnifying lens is used. Accordingly,  
20 it is necessary to increase the number of ribbons of the GLV 32 in order to widen the horizontal length of the stereoscopic image. However, the yield of manufacturing is decreased and the manufacturing cost increased when the device area of the GLV 32 is enlarged.

25

~~Accordingly, it is necessary to increase the number of ribbons of the GLV 32 in order to widen the horizontal length of the stereoscopic image. On the other hand, the yield of manufacturing may be decreased and the manufacturing cost may~~

~~be increased if the device area of the GLV 32 is to be enlarged.~~

Because When, in the display apparatus 30, the laser beams are scanned by the first and the second  
5 galvano-mirrors 34,35 in the horizontal direction and in the vertical direction. ~~Namely~~, the laser beams are, so to speak, two-dimensionally scanned. Accordingly, the horizontal length of the stereoscopic image to be  
10 length of the ribbon arrays 32a, 32b, 32c formed on the GLV 32.

When the operation frequencies of the first and the second galvano-mirrors 34, 35 are 1 MHz, 200 lines  
15 may be scanned by the first galvano-mirror 34 in the horizontal direction even if 5,000 lines are scanned by the second galvano-mirror 35 in the vertical direction. Accordingly, ~~as described above~~, when the GLV 32 on which 6,144 ribbons are formed with intervals of 5 [[lm]]  $\mu\text{m}$   
20 between each other is used, the horizontal length of the stereoscopic image to be displayed may be enlarged up to 6 m.

Because the amount of information to be processed  
25 naturally increases ~~by leaps and bounds~~ considerably for the displaying of a stereoscopic image in a large size as described above, the ~~practically~~ realizable image size is limited depending on the performance of signal processing. The display apparatus 30 according to the

present embodiment is ~~sufficiently~~ capable of displaying a stereoscopic image in the aforesaid ~~degree~~ of size. By ~~alleviating the limitation due to the~~ improving signal processing capability by, for example, 5 utilizing a parallel processing technique of a high performance computer apparatus ~~having high operation performance~~, an extra-large three-dimensional image may also be displayed.

10 It is difficult to scan the laser beams precisely in the horizontal direction and in the vertical direction as shown in Fig. 6 because the first and the second galvano-mirrors 34, 35 are driven to rotate continuously in the present embodiment. Alternatively, 15 by changing the ~~change of~~ scanning speeds of the first and the second galvano-mirrors 34, 35 in the display apparatus 30 ~~as shown in Fig. 7~~, laser beams may be scanned obliquely, as shown in Fig. 7. More specifically, for example, the laser beam may be scanned 20 six times in the vertical direction by the second galvano-mirror 35 while the laser beam has been scanned once in the horizontal direction by the first galvano-mirror 34. However, because the one-dimensionally modulated laser beam is shifted in the 25 horizontal direction while the laser beam is scanned in the vertical directions in this case, an amount of such shifting should be ~~in~~ taken into consideration ~~to drive~~ for driving the ribbon arrays 32a, 32b, 32c of the GLV 32.

In the display apparatus 30, by the aforesaid operation of the first and the second galvano-mirrors 34, 35, the laser beams are scanned in the horizontal direction and the vertical direction. Then, the scanned laser beams ~~is~~ are incident on the Fourier transformation lens 36. Other types of lens may be employed in place of the Fourier transformation lens 36 as long as such lens can perform Fourier transformation on the desired light. The Fourier transformation lens 36 alters the laser beams passing through it according to the Fourier transformation. Then, the transformed laser beams are incident on the one-dimensional diffuser panel 37.

15

~~The Fourier transformation lens 36 makes the incident laser beams pass through it to transform them by the Fourier transformation. Then the Fourier transformation lens 36 makes the transformed laser beams be incident on the one dimensional diffuser panel 37.~~

20

~~Alternatively, other types of lens may be employed in place of the Fourier transformation lens 36 as long as such lens can perform Fourier transformation on the desired light.~~

25

The one-dimensional diffuser panel 37 is disposed on a Fourier surface of the Fourier transformation lens 36[[,]] and ~~the one dimensional diffuser panel 37 makes~~ diffuses the incident laser beams ~~pass~~ passing through it ~~to diffuse them~~

one-dimensionally. Because the display apparatus 30 is provided with the one-dimensional diffuser panel 37, ~~the display apparatus 30~~ a slightly enlarges the enlarged visual field ~~thereof~~ is obtainable in the vertical direction, and  
5 which can make the discontinuities between the wavefronts of the laser beams ~~that are~~ scanned in the vertical directions inconspicuous, thereby realizing more natural stereoscopic effects. After passing through the one-dimensional diffuser panel 37, the laser beams are projected on a projection plane  
10 and a stereoscopic image G having horizontal parallax is displayed, as shown in Fig. 4.

~~Then, in the display apparatus 30, the laser beams passed through the one dimensional diffuser panel 37 is projected on a projection plane as shown in Fig. 4, and a stereoscopic image G having horizontal parallax is displayed.~~

15

The display apparatus 30 comprises a control circuit 40, as shown in Fig. 8. The control circuit 40 ~~is constituted~~  
20 by includes, for example, various semiconductor devices. The information (hereinafter referred to as display image data) concerning stereoscopic images to be displayed is input into the control circuit 40. The information may be from an apparatus ~~that may be~~ located outside the display apparatus  
25 30. The control circuit 40 controls the GLV 32 according to the input display image data to drive the plural ribbons formed on the GLV 32 separately. Moreover, the control circuit 40 controls the rotation speeds and the rotation timings of the first and the second galvano-mirrors 34, 35.



The control circuit 40 ~~is~~ can comprise, for example ~~as shown in Fig. 8,~~ comprises a clock generator 41, a Fourier transformation section 42, a GLV driving section 43, and a galvano-mirror driving section 44. The clock generator 41 generates a clock signal for referencing the operation timing of the control circuit 40 and the whole operation timing of the display apparatus 30. The clock generator 41 outputs the generated clock signal to the GLV driving section 43 and the galvano-mirror driving section 44. The signal level of the clock signal can be set to change in a predetermined manner. Each section of the control circuit 40 performs various kinds of processing at the timing of the signal level change of the clock signal.

~~The clock generator 41 generates a clock signal being a reference of the operation timing of the control circuit 40, and the whole operation timing of the display apparatus 30. The clock generator 40 outputs the generated clock signal to the GLV driving section 43 and the galvano-mirror driving section 44. The signal level of the clock signal changes, for example, every predetermined time. Each section of the control circuit 40 performs various kinds of processing at the timing of the signal level change of the clock signal.~~

The Fourier transformation section 42 receives display image data from an external apparatus, and performs the Fourier transformation processing of the display image data.

Then, the Fourier transformation section 42 outputs the data after performing the Fourier transformation processing to the GLV driving section 43.

5           The GLV driving section 43 operates at a timing based on the clock signal input from the clock generator 41, and controls the GLV 32 in accordance with the data input from the Fourier transformation section 42. That is, the GLV driving section 43 drives each ribbon formed on the GLV 32  
10 to ascend or to descend, and sets each ribbon array 32a, 32b, 32c of the GLV 32 at a desired position that corresponds to a phase distribution in accordance with the input data.

          The galvano-mirror driving section 44 controls the  
15 rotations of the first and the second galvano-mirror 34 according to the timing based on the clock signal input from the clock generator 41.

~~The control circuit 40 has the following control~~  
20 ~~function.~~ That is, by the operation of the GLV driving section 43 and the galvano-mirror driving section 44 according to the clock signal, the control circuit 40 ~~makes~~ causes the GLV 32 and the first and the second galvano-mirrors 34, 35 to operate at suitable timings in cooperation with each  
25 other. When the laser beams are scanned under the ~~above-cited~~ control of the control circuit 40, ~~an~~ a stereoscopic image is displayed in the display apparatus 30<sub>L</sub> as shown in Fig. 6 or Fig. 7.

The display apparatus 30 structured in such a way uses a micromachine type one-dimensional spatial modulator, i.e. the GLV 32, as a spatial modulator for modulating light to be projected. Because the GLV 32 can be operated at an extremely high speed, an abundant amount of information may be used to display the stereoscopic image ~~may be displayed while using sufficiently abundant amount of information.~~ Moreover, because the display apparatus 30 displays the stereoscopic image with the light modulated by the GLV 32, the overall structure of the apparatus may be simplified, and the manufacturing cost thereof may be lowered. Moreover, stereoscopic effects may be expressed without using special equipment such as dedicated glasses for viewing a stereoscopic image.

15

Moreover, the display apparatus 30 modulates the laser beams with the GLV 32 having a function of ~~an~~ a one-dimensional spatial modulator~~[[,]]~~ and projects the modulated laser beams while scanning them to predetermined directions. Thereby, the display apparatus 30 displays the stereoscopic image. That is, the display apparatus 30 relinquishes the vertical parallax in the stereoscopic image to be displayed~~[[,]]~~ and displays the stereoscopic image only with its horizontal parallax. Since the display apparatus 30 displays the stereoscopic image by utilizing only the horizontal parallax, the display apparatus 30 may suppress the increase of the amount of information necessary for displaying the stereoscopic image. ~~and thereby~~ Thereby, it becomes possible to decrease the amount of information and ~~the~~ processing time.

~~both being~~ necessary for displaying the stereoscopic image.

In the above description, the display apparatus 30 scans the laser beams in the horizontal direction and in the vertical direction ~~with~~ using the first and the second galvano-mirrors 34, 35, ~~and consequently~~. In this way, the display apparatus 30 functions, so to speak, as a scan mechanism for scanning the laser beams.

10 The display apparatus 30 is not limited to ~~be being~~ equipped with the scan mechanism structured ~~in such a way as~~ described. ~~Alternatively, any~~ Any scan mechanism structured to scan and project laser beams in predetermined directions may be ~~employable~~ used. More specifically, for example, the  
15 scan mechanism may be structured by the use of a two-axis galvano-mirror having rotational axes orthogonal to each other and able to be driven two-dimensionally.

~~More specifically, for example, the scan mechanism may~~  
20 ~~be structured by the use of a two-axis galvano-mirror that is equipped with rotational axes orthogonal to each other and may drive a mirror two-dimensionally.~~

Moreover, ~~still as~~ as another type of the scan mechanism,  
25 a mirror array 50, as shown in Fig. 9, may be used. In the mirror array 50, ~~as shown in Fig. 9,~~ surfaces on which the laser beams are incident upon are formed in a multistage shape. The reflection angle of each stage mirror is formed to differ from each other slightly. Then, by the use of the mirror array

50 in combination with, for example, the first galvano-mirror 34, the scanning with the scan mechanism is accomplished. In this case, for example, by rotating the galvano-mirror 34 about the horizontal axis, the laser beams are scanned in the direction of an arrow A (i.e., in the vertical direction). Then, the laser beams are incident on the reflection surfaces of the mirror array 50 and scanned in the direction of an arrow B in Fig. 9, namely the direction of a combination of the vertical direction and the horizontal direction, on a projection plane 51.

~~In this case, for example, by the rotation driving of the galvano mirror 34 about the horizontal axis, the laser beams are scanned in the direction of an arrow A in Fig. 9, i.e. the vertical direction. Then, the laser beams are incident on the reflection surfaces of the mirror array 50, and thereby the laser beams are scanned in the direction of an arrow B in Fig. 9, namely the direction of a combination of the vertical direction and the horizontal direction, on a projection plane 51.~~

Moreover, in the display apparatus 30, the scan mechanism may be structured by the combination of, for example, a polygon mirror and a volume type hologram. Alternatively, the display apparatus may be structured to scan the laser beams by the rotation of the GLV 32 itself with utilizing a rotation mechanism such as a stepping motor.

Although the invention has been described in its

preferred ~~form~~ forms with a certain degree of particularity,  
~~obviously many~~ changes, variations, and combinations of the  
embodiments are possible therein. It is therefore to be  
understood that the present invention may be practiced other  
5 than as specifically described herein without departing from  
the scope of the invention ~~thereof~~.

What is claimed is:

1. (Currently amended) A stereoscopic image display apparatus comprising:
  - a light source radiating light of a wavelength in
  - 5 a predetermined wavelength range;
  - a one-dimensional spatial modulator ~~configured to generate an arbitrary phase distribution using~~ including one-dimensionally arrayed elements having top surfaces, the elements being that are independently driven such that the
  - 10 entire top surface of each element selectively moves upward and downward during operation of the display apparatus; and
  - a scan unit scanning the light to a predetermined direction during operation of the display apparatus to ~~display a stereoscopic image,~~ the light being from said light
  - 15 source, having entered into said one-dimensional spatial modulator and having been modulated therein.
2. (Currently amended) The stereoscopic image display apparatus according to claim 1, wherein said scan unit scans the light modulated by said one-dimensional spatial

modulator in a direction perpendicular to an arraying direction of the elements of said one-dimensional spatial modulator to achieve horizontal parallax.

3. (Currently amended) The stereoscopic image display apparatus according to claim ~~[[1]]~~ 2, wherein ~~said light source is provided with laser oscillators radiating laser beams having wavelengths in predetermined wavelength ranges severally corresponding to red, green and blue~~ said scan unit is a first scan unit rotating about a first scan unit axis and the apparatus further comprises a second scan unit rotating about a second scan unit axis orthogonal to the first scan unit axis, the second scan unit scanning the modulated light in a direction parallel to an arraying direction of the elements of said one-dimensional spatial modulator to achieve vertical parallax.

4. (Previously presented) The stereoscopic image display apparatus according to claim 1, said apparatus further comprising:

a diffuser panel diffusing modulated light scanned



by said scan unit to display the stereoscopic image.

5. (Original) The stereoscopic image display apparatus according to claim 1, wherein said one-dimensional spatial modulator comprises a Grating Light Valve.

5 6. (Currently amended) A stereoscopic image display apparatus comprising:

a light source radiating light having a wavelength in a predetermined wavelength range;

a Grating Light Valve device ~~having~~ including a  
10 plurality of ribbon-like elements having top surfaces, the  
Grating Light Valve being and configured to generate an  
~~arbitrary~~ a phase distribution by independently driving each  
ribbon-like element so that all of the top surface of each  
element selectively moves up and down during operation of the  
15 display apparatus;

a collimator lens making the light modulated by  
said Grating Light Valve device into parallel ~~ray~~ rays;

a scan unit scanning the parallel ~~ray~~ rays coming  
from said collimator lens;

a lens performing Fourier transformation on the scanned ~~ray~~ rays; and

a diffuser panel diffusing the ~~ray~~ Fourier transformed rays by said lens ~~to display a stereoscopic image.~~

5           7. (Currently amended) A stereoscopic image display apparatus comprising:

means for radiating coherent light;

means for ~~generating an arbitrary phase distribution by~~ spatially modulating the coherent light in  
10 a one-dimensional direction, wherein the means for spatially modulating is controlled in part according to a Fourier transformation function; and

means for scanning the modulated light in ~~to~~ a ~~predetermined~~ direction orthogonal to said one-dimensional  
15 direction and in a direction parallel to said one-dimensional direction ~~to display a stereoscopic image.~~

8. (Currently amended) A stereoscopic image display method comprising:

radiating coherent light;

~~generating an arbitrary phase distribution by~~  
spatially modulating the coherent light in a one-dimensional  
direction in accord with a Fourier transformation function;  
and

5       ~~displaying a stereoscopic image by~~ scanning the  
modulated light to a ~~predetermined~~ direction orthogonal to  
said one-dimensional direction at a first speed.

9. (New) A stereoscopic image display apparatus  
according to claim 1, wherein the scan unit is a polygon mirror  
10 and the apparatus further comprises a volume type hologram  
device.

10. (New) A stereoscopic image display apparatus  
according to claim 2, wherein the scan unit is a  
galvano-mirror and the apparatus further comprises a  
15 multistage mirror having a plurality of stacked reflection  
surfaces, wherein each surface has an angle that is different  
than angles of the other of said reflection surfaces, for  
scanning the light scanned by the scan unit in a direction  
intermediate said perpendicular direction to the arraying

direction of the elements of said one-dimensional spatial modulator and parallel to the arraying direction of the elements.

11. (New) A stereoscopic image display apparatus  
5 according to claim 3, wherein the first and second scanning units are galvano-mirrors.

12. (New) A stereoscopic image display method according to claim 11, further comprising:

a collimator lens to parallelize the modulated  
10 light before scanning by the first and second scanning units during operation of the display apparatus; and

a Fourier transformation lens for transforming the modulated, parallelized, and two-dimensionally scanned light during operation of the display apparatus.

13. (New) A stereoscopic image display method  
15 comprising according to claim 8, further comprising:

scanning the modulated light to a direction parallel to said one-dimensional direction at a second speed that is different than said first speed, wherein said spatial

modulation is controlled based on an amount of shifting of the scanned light resulting from said differing scanning speeds.

14. (New) A stereoscopic image display method  
5 according to claim 8, wherein:

the spatial modulation is performed with a modulation device; and  
the modulation device rotates during performance of the method.

## ABSTRACT OF THE DISCLOSURE

A stereoscopic image display apparatus is provided. The apparatus comprises a light source radiating light with a predetermined wavelength range, an one-dimensional spatial modulator including one-dimensionally arranged elements  
5 that are independently driven to generate an arbitrary phase distribution, and a scan unit scanning the light from the light source to a predetermined direction, the light having entered into the one-dimensional spatial modulator and  
10 having been modulated therein.